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# An in situ probe-spacing-correcting thermo-TDR sensor to measure soil water content accurately

## Abstract

To reduce the possibility of probe deflections, conventional thermo-time domain reflectometry (T-TDR) sensors have relatively short probe lengths ( $\leq 4$  cm). However, short probes lead to large errors in TDR-estimated soil water content ( $\theta_v$ ). In this study, two new 6-cm-long probe-spacing-correcting T-TDR (CT-TDR) sensors were investigated. Compared to conventional 4-cm-long T-TDR sensors, the 6-cm-long CT-TDR sensors reduced errors in TDR-estimated  $\theta_v$ . Errors in heat pulse (HP) estimated  $\theta_v$  because of probe deflections were reduced when linear or nonlinear probe spacing correcting algorithms were implemented. The 6-cm-long CT-TDR sensors provided more accurate  $\theta_v$  estimations than do the conventional 4-cm-long T-TDR sensors.

## Keywords

probe deflection, probe length, probe spacing changes

## Disciplines

Agricultural Science | Hydrology | Soil Science

## Comments

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**An *in situ* probe-spacing-correcting thermo-TDR sensor to measure soil water  
content accurately**

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*Running Title: Probe-spacing-correcting thermo-TDR sensor*

## Summary

To reduce the possibility of probe deflections, conventional thermo-time domain reflectometry (T-TDR) sensors have relatively short probe lengths ( $\leq 4$  cm). However, short probes lead to large errors in TDR-estimated soil water content ( $\theta_v$ ). In this study, two new 6-cm-long probe-spacing-correcting T-TDR (CT-TDR) sensors were investigated. Compared to conventional 4-cm-long T-TDR sensors, the 6-cm-long CT-TDR sensors reduced errors in TDR-estimated  $\theta_v$ . Errors in heat pulse (HP) estimated  $\theta_v$  because of probe deflections were reduced when linear or nonlinear probe spacing correcting algorithms were implemented. The 6-cm-long CT-TDR sensors provided more accurate  $\theta_v$  estimations than do the conventional 4-cm-long T-TDR sensors.

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*Keywords: probe deflection, probe length, probe spacing changes.*

**Highlights:**

- Short thermo-TDR sensor has shortcomings in determining soil water content.
- Changes in thermo-TDR probe spacing caused by deflections can be determined *in situ*.
- Correcting changed thermo-TDR probe spacing determines soil water content accurately.
- The 6-cm long thermo-TDR sensors determined soil water content more accurately than 4-cm long sensors.

## Introduction

Soil water content and thermal properties are important for soil surface energy partitioning and for subsurface heat and water transfer. Time domain reflectometry (TDR) is widely used to determine soil water content ( $\theta_v$ ) (Robinson *et al.*, 2008). The heat pulse (HP) method can determine thermal properties of soil (Bristow *et al.*, 1994) and  $\theta_v$  (Heitman *et al.*, 2003). To determine  $\theta_v$  and thermal properties simultaneously, Noborio *et al.* (1996) and Ren *et al.* (1999) developed the thermo-time domain reflectometry (T-TDR) sensor by combining HP and TDR sensors. The T-TDR sensor can also be used to determine soil bulk density (Ochsner *et al.*, 2001).

There is a conflict between the optimal probe length for HP and TDR sensors. Dalton & van Genuchten (1986) recommend that TDR probes be at least 10-cm long, because probe length can affect the accuracy of waveform analysis, and shorter probes have relatively large uncertainties in estimating  $\theta_v$  (Heimovaara, 1993). Commonly used HP probes have a diameter of  $\leq 1.27$  mm. Unaccounted for changes in probe spacing ( $r$ ) can lead to errors in estimated specific heat ( $c$ ) values (Wen *et al.*, 2015). To minimize the possibility of changes in  $r$  because of deflections, the majority of HP probes are relatively short ( $\leq 4$  cm). Therefore, most T-TDR probes are 4-cm-long or less. Short T-TDR probes, however, are not as accurate as long probes for determining  $\theta_v$ .

Several methods are available to improve the performance of T-TDR sensors. Using an expensive cable tester or oscilloscope with a short rise time ( $\leq 200$  ps) (Kelly *et al.*, 1995) and performing data smoothing and filtering analysis on the waveforms (Wang *et al.*, 2016) can improve TDR waveform analysis for short probes. To minimize probe deflection, Kamai *et al.* (2015) made robust probes by increasing their diameter. Compared with thin probes, however, thick probes can compact soil

(Rothe *et al.*, 1997) and distort water flow around the probes (Hinnell *et al.*, 2006).

*In situ* probe-spacing-correcting HP sensors can correct linear (Liu *et al.*, 2013) and nonlinear probe deflections (Liu *et al.* 2016). If the correcting methods can be introduced effectively into T-TDR sensors with relatively long TDR probes, then,  $r$  can be determined accurately and errors in  $c$  and  $\theta_v$  can be reduced. In addition, the accuracy of TDR-estimated  $\theta_v$  with the longer T-TDR sensor will be improved.

In this study, we evaluated how accurately *in situ* probe-spacing-correcting T-TDR (CT-TDR) sensors (Figure 1a) with probe lengths of 6 cm could determine  $\theta_v$  derived from TDR waveforms, and from HP we estimated soil specific heat.

## Theory

### *The heat pulse (HP) method*

The HP estimated  $\theta_v$  is calculated as (Campbell *et al.*, 1991):

$$\rho c = \rho_b c_s + \rho_w c_w \theta_v, \quad (1)$$

where  $\rho_w$  (kg m<sup>-3</sup>) and  $\rho_b$  (kg m<sup>-3</sup>) are the water density and soil bulk density, respectively, and  $c_s$  (J kg<sup>-1</sup> K<sup>-1</sup>) and  $c_w$  (J kg<sup>-1</sup> K<sup>-1</sup>) are the specific heat of soil solids and water, respectively. The product  $\rho c$  (J m<sup>-3</sup> K<sup>-1</sup>) is equal to the soil volumetric heat capacity ( $C$ ).

*Probe-spacing-correcting method.* The linear model described by Liu *et al.* (2013) for the nonlinear model described by Liu *et al.* (2016) for linear and nonlinear probe deflection, respectively, are used for probe-spacing-correction.

### *The TDR method*

An empirical relation between  $\theta_v$  and  $K_a$  (dielectric constant of soil) (Topp *et al.*, 1980) is used to calculate  $\theta_v$

$$\theta_v = -5.3 \times 10^{-2} + 2.92 \times 10^{-2} K_a - 5.5 \times 10^{-4} K_a^2 + 4.3 \times 10^{-6} K_a^3. \quad (2)$$

## Materials and methods

In this study, we carried out both HP and TDR measurements to test the application of the *in situ* CT-TDR sensor.

#### *Heat pulse experiments*

The 6-cm-long CT-TDR sensors used in this study had a probe diameter of 1.27 mm. Two kinds of 6-cm-long sensors were investigated: Sensor T6A (two thermistors ( $l$ ) in each temperature probe,  $l_1=4$  cm and  $l_2=2$  cm) and Sensor T6B (three thermistors in each temperature probe,  $l_1=4.5$  cm,  $l_2=3$  cm and  $l_3=1.5$  cm). Based on the results of Wen *et al.* (2015) and the strain relationship for a bar (Beer *et al.*, 2006), Sensors T6A and T6B were used to test the linear and nonlinear models, respectively.

The HP experiments were performed on sand samples with known  $\rho_b$  over a wide range of  $\theta_v$  ( $c_s=751$  J kg<sup>-1</sup> K<sup>-1</sup> measured by differential scanning calorimetry (DSC) at 20°C). Additional details about probe deflection and HP measurements can be found in Wen *et al.* (2015).

#### *The TDR experiments*

Two types of TDR sensors were investigated: two 4-cm-long T-TDR sensors (T4A and T4B) and two 6-cm-long CT-TDR sensors (T6A and T6B). All the TDR sensors had a three-probe design. The TDR measurements were made at variable  $\theta_v$  with known  $\rho_b$  in sandy clay soil and in sand, and waveforms were recorded by a TDR100 (Campbell Scientific, Inc. Logan, UT). The actual volumetric  $\theta_v$  of each sample was determined by oven-drying to measure the gravimetric  $\theta_v$  and multiplying the gravimetric value by the sample  $\rho_b$ . The actual  $\theta_v$  values were used as the reference volumetric  $\theta_v$  ( $\theta_{v\_ref}$ ).

## **Results and discussion**

#### *Heat pulse results*

The HP-estimated  $\theta_v$  values are presented in Figure 2; each value represents the average value derived from the two (for the linear model) or three (for the nonlinear model) thermistors in each temperature probe.

Figure 2 shows that, without corrections for  $r$ , deflections can cause large errors in the estimated  $\theta_v$  values. The corrected  $\theta_v$  values derived from the linear and nonlinear models are much closer to the actual  $\theta_{v\_ref}$  values than are the uncorrected values.

For the linear model, we obtained a regression equation of

$$Y = 0.902 X + 0.007 \quad (R^2 = 0.826),$$

whereas for the nonlinear model, we obtained a regression equation of

$$Y = 0.981 X + 0.005 \quad (R^2 = 0.982).$$

These regression results indicate that the nonlinear model was more accurate than the linear model. However, the nonlinear model uses three thermistors, which requires several datalogger channels per sensor. In some situations, it may be advantageous to use the linear model which does not use as many channels.

Probe deflections caused larger errors in  $\theta_v$  than in  $c$  ( $c$  data not shown), even after the  $r$  values were corrected. According to Heitman *et al.* (2003), errors in  $\theta_v$  for the heat pulse method are due to a combination of parameters such as  $c_s$ ,  $r$ ,  $q$  (the energy input per unit length of heater per unit time of the HP sensor) and  $\Delta T_m$  (the maximum temperature rise of the temperature curve). A change in  $r$  is just one of the sources of error in  $\theta_v$ , so although  $r$  is corrected, errors in HP-estimated  $\theta_v$  remain.

### *The TDR results*

The TDR-estimated  $\theta_v$  values ( $TDR\theta_v$ ) are shown in Figure 3. Results indicate that the accuracy of TDR-estimated  $\theta_v$  increases with increasing probe length. The  $R^2$  value for the 6-cm-long TDR probes (0.960) was larger than that for the 4-cm-long TDR



probes (0.912). For a 5-cm-long TDR probe, Topp *et al.* (1984) reported an  $R^2$  value of 0.957, which is between the values for our 4- and 6-cm-long probes. The difficulty in detecting the reflection points in a short probe TDR waveform (Heimovaara, 1993) might account for the relatively large errors and scattered data points for the 4-cm-long probes.

Although long TDR probes provided better estimates of  $\theta_v$  than short ones, it does not mean that the longer is the probe length, the better is the performance of CT-TDR sensors. This is because long probes are more apt to deflect than short probes. In addition, the probe-spacing-correcting method relies on the assumption that soil is homogeneous. Therefore, in strongly heterogeneous soil, long probes might be more vulnerable to errors than short probes.

## Conclusions

We introduced a new 6-cm-long CT-TDR sensor that combined the TDR and *in situ* probe-spacing-correcting HP methods. The HP results indicated that, after *in situ* probe-spacing corrections, sensors provided more accurate results than those that were uncorrected. The TDR results indicated that 6-cm-long TDR probes were more accurate than 4-cm-long TDR probes. The 6-cm-long CT-TDR sensor improved on shortcomings of the 4-cm-long T-TDR sensor.

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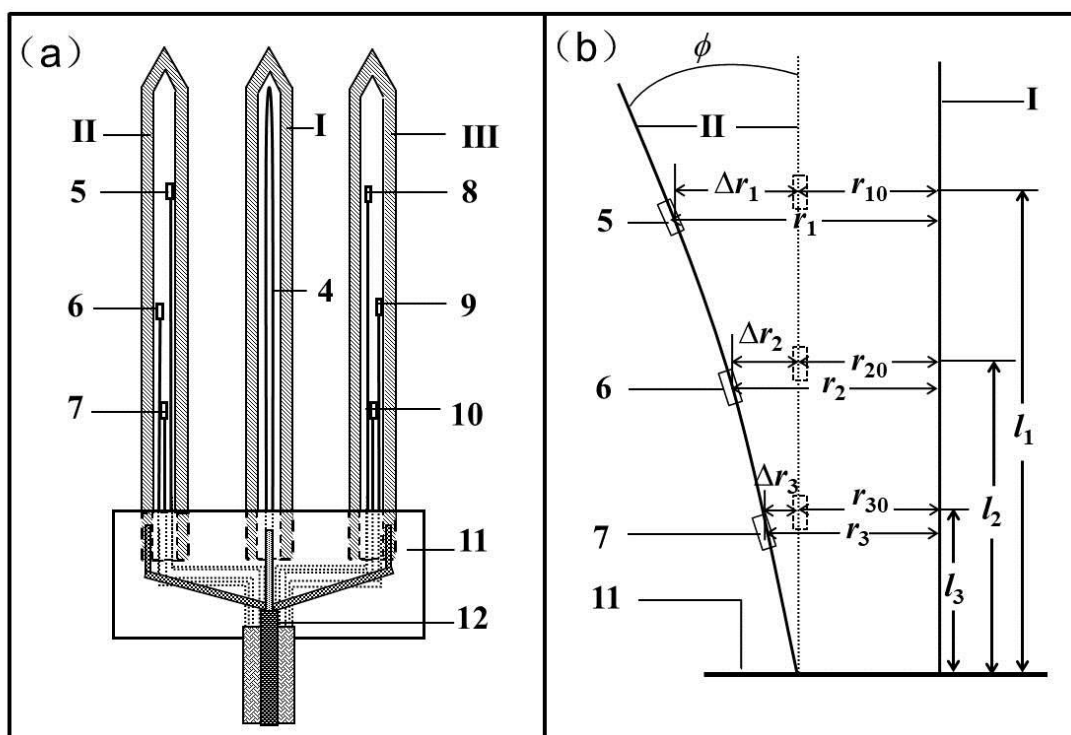
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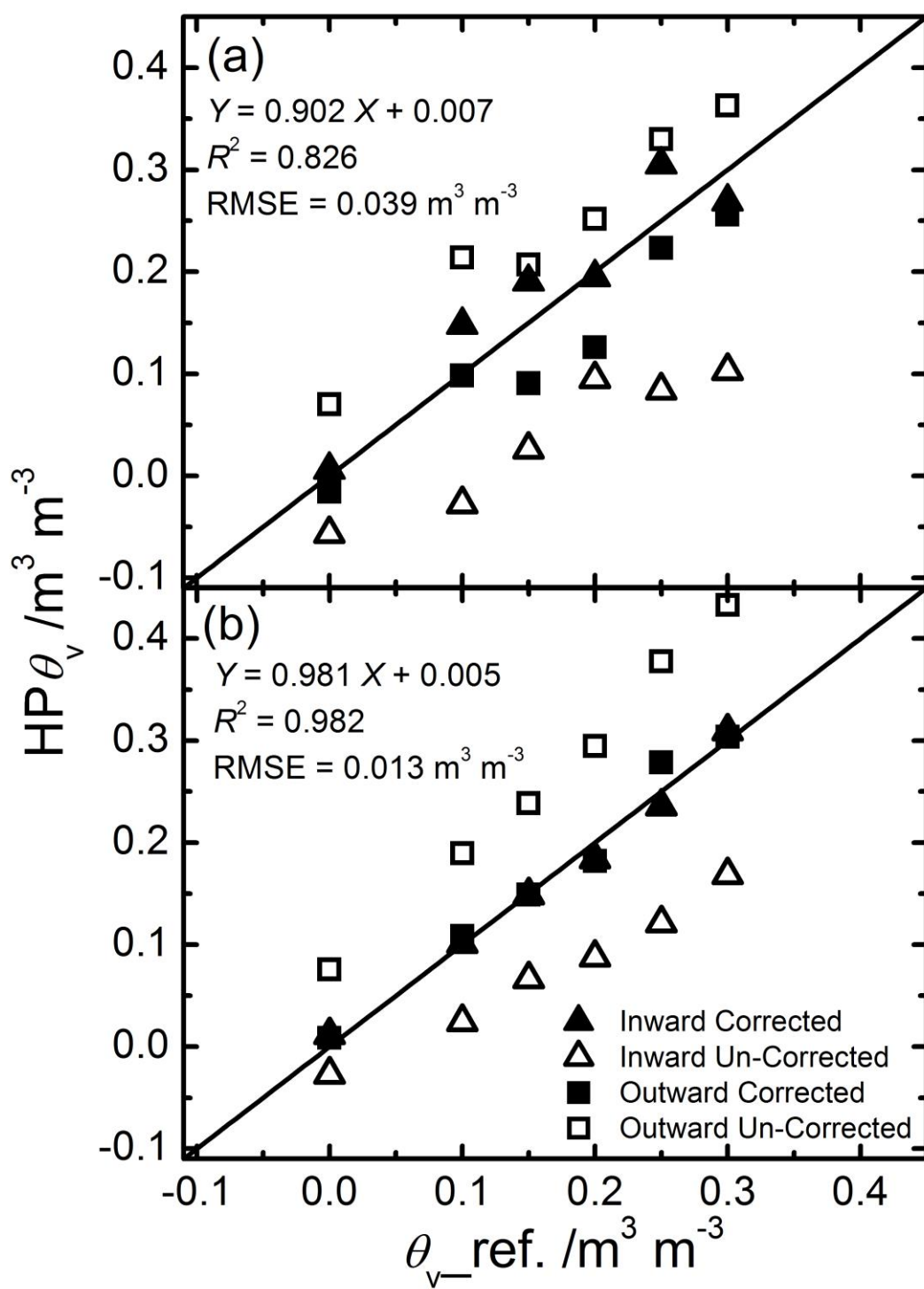
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# FIGURE CAPTIONS

**Figure 1** (a) Side view of the cross section of the probe-spacing-correcting thermo-TDR (CT-TDR) sensor and (b) diagram for a deflected CT-TDR sensor (nonlinear outward deflection). I, Heating probe; II and III, temperature probes; 4, heating wire; 5–10, thermistors (5, thermistor 1; 6, thermistor 2; 7, thermistor 3; 8, thermistor 4; 9, thermistor 5; 10, thermistor 6); 11, epoxy plug; 12, coaxial cable;  $\phi$ , deflected angle;  $l_i$ , the distance of thermistor  $i$  to the surface of epoxy plug;  $r_{i0}$ , initial probe spacing for thermistor  $i$ ;  $r_i$ , the changed probe spacing for thermistor  $i$ ;  $\Delta r_i$ , The displacement of thermistor  $i$ .



**Figure 2** (a) Heat-pulse estimated water content values ( $HP\theta_v$ ) plotted against actual values of reference volumetric water content ( $\theta_{v\_ref.}$ ) for sand corrected with linear model and (b) heat-pulse estimated water content values ( $HP\theta_v$ ) plotted against actual values of reference volumetric water content ( $\theta_{v\_ref.}$ ) for sand corrected with nonlinear model. The black solid line is the 1:1 line.





**Figure 3** (a) The TDR estimated water content ( $\text{TDR}\theta_v$ ) for sand and sandy clay by T4 probes and (b) the TDR estimated water content ( $\text{TDR}\theta_v$ ) for sand and sandy clay by T6 probes plotted against reference volumetric water content values ( $\theta_{v\_ref.}$ ). The black solid line is the 1:1 line and the dashed lines enclose a 95% prediction interval.

